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## METHOD AND APPARATUS FOR SECURE ULTRAFAST COMMUNICATION

### RELATED APPLICATION

Priority is claimed from U.S. Provisional Patent Application Number 60/253,288, filed November 27, 2000, and said U.S. Provisional Patent Application is incorporated herein by reference.

### BACKGROUND OF THE INVENTION

Optical techniques have previously been suggested for information security [see, for example, Appl. Opt. 32:5026 (1993); Opt. Eng. 33:1752 (1994); Opt. Lett. 20:767 (1995); and Opt. Lett. 23:1483 (1998)]. Encrypted holographic memory systems have previously been demonstrated for retrieving information for authorized users [see Opt. Lett. 24:762 (1999)]. In these systems two random phase masks located at the input and Fourier planes convert an original image into a random-noise-like image. A correct random phase key is required for successful retrieval of the original data. This encrypted

holographic memory potentially has a large storage capacity with a fast access; thus it can be used as an encrypted database.

Pulse shapers based on Fourier synthesis in the temporal frequency domain have previously been thoroughly investigated [see, for example, Appl. Phys. B 50:101 (1990); IEEE J. Quantum Electron 28:2251 (1992); Opt. Lett. 19:664 (1994); Appl. Opt. 37:2858 (1998); and J. Opt. Soc. Am. A 16:1076 (1999)]. For secure communications A. W. Weiner et al. [see IEEE J. Quantum Electron 28:2251 (1992)] proposed a technique based on spectral phase coding for encryption and decryption of femtosecond pulses. This technique can be used in a code-division multiple-access network. Pulse shapers (or spatial-temporal converters) can be used to send spatial data to remote users at ultrahigh speeds as great as terabit(s).

It is among the objects of the present invention to provide an ultrafast data communication system that can link remote users to an encrypted database with high security and ultrafast transfer rate.

## SUMMARY OF THE INVENTION

In accordance with a form of the invention, an ultrafast secure data communication system and method is set forth that can link remote users to an encrypted database with high security and ultrafast transfer rate. A data storage method and system is also set forth.

In an embodiment of the present invention, all data are stored holographically in a storage medium such as conventionally used photorefractive materials or photopolymers after the original data is encrypted in the spatial domain with double-random phase encryption [see Opt. Lett. 20:767 (1995)]. Each encrypted spatial datum can be sent to the receivers at ultrahigh speed with spatial-temporal converters. At each receiver the temporal data are converted back into spatial data, and the original data can be reconstructed when tested by use of a correct random phase key. If one should use an incorrect key, the reconstructed data will remain as a random-noise like image, owing to the nature of double-random phase encryption. An embodiment of the invention uses double-random phase encryption and is more secure than the spectral phase coding system in which only one random phase mask was used in the Fourier plane, because a phase-retrieval algorithm cannot be used to reconstruct the data.

An embodiment of the present invention is directed to an ultrafast secure data communications system and method that uses spatial-temporal converters. In this system and method, the original spatial signal is optically encrypted, and the encrypted signal is holographically stored in a storage medium such as a photoreactive material. The spatially encrypted signal is sampled to avoid the overlap of each datum at the receiver. The sampled data are converted into a temporal signal in order

to transmit the information through an optical fiber. At the receiver-end, the temporal signal is converted back into the initial spatially encrypted signal. Retrieval of the original data can then be achieved when the correct phase key is used in a decryption system. A feature hereof is the development of an expression of encrypted output and decrypted data.

In studies by Marcom et al. [see Appl. Opt. 37:2858 (1998)], it was pointed out that the spatial data sent by spatial-temporal converters broadens because the point-spread function of the system is dependent on the input pulse width. Thus, they concluded, encrypted data at the transmitter should be sampled to avoid the overlap between adjacent pixels at the receiver-end that are due to the point-spread function caused by the pulse width of input light. In view of these prior reports, and as described further hereinbelow, the system described herein was analyzed to provide a numerical evaluation of the effect of sampling of the spatially encrypted data on the quality of the reconstructed data.

In accordance with an embodiment of the technique of the invention, a method is set forth for securely communicating information, comprising the following steps: optically encrypting said information and storing the resulting encrypted data; reading out the encrypted data in the spatial domain, and converting said encrypted data to the temporal domain; transmitting the converted encrypted data; receiving the transmitted encrypted data and converting the received encrypted data to the spatial domain; and decrypting the converted received encrypted data to recover said information. In a preferred form of the invention, the step of reading out the encrypted data in the spatial domain and converting the encrypted data to the temporal domain is implemented using ultrafast laser pulses.



## BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 illustrates the encryption optical memory system, both at the transmitted-end and receiver-end, according to an embodiment of the present invention using spatial-temporal converters and double-random phase encoding;

FIG. 2 depicts an encrypted memory system comprising the recording (a) and readout (b) components according to an embodiment of the present invention;

FIG. 3 depicts an encryption transformer using a space-to-time converter in accordance with an embodiment of the present invention;

FIG. 4 depicts a receiver using a time-to space converter in accordance with an embodiment of the invention;

FIG. 5 depicts the decryption system according to an embodiment of the invention utilizing a phase key for decryption;

FIG. 6 is a graphic representation of the mean-square errors between original and reconstructed data with low-pass filtration as a function of the sampling interval  $\Delta$ ;

FIG. 7 depicts examples of original digital data, encrypted data and reconstructed data in which (a) depicts the original digital data and the encrypted data and (b) depicts the original digital data and the reconstructed data (low-pass filtered) when the sampling interval,  $\Delta$ , is 2; and

FIG. 8 graphically depicts the bit error rate of binarized reconstructed data as a function of the sampling interval,  $\Delta$ .

## DETAILED DESCRIPTION

An illustration of the proposed ultrafast secure data communication system and method according to an embodiment of the invention is shown in FIG. 1. The proposed system comprises four subsystems, which are (1) an optically encrypted memory system, (2) a transmitter to convert the encrypted data into temporal data with a space-to-time converter, (3) a receiver to convert the temporal data into the encrypted data with a time-to-space converter, and (4) an optical decryption system. Each individual subsystem is more fully described below.

In the embodiment of Figure 1, an encrypted memory system 200 (for example, the system of Figure 2) receives input information (for example, images or text) and stores encrypted data in optical storage medium 210, for example holographic optical storage. The data read out of optical storage 210 and a reference beam from a laser (not shown) are input to interferometric optical processing, represented as including splitter 225 and lens L2, to obtain real time hologram at a storage medium 240, such as a multiple quantum well photorefractive device or higher order material. A pulsed laser 245 produces ultrafast input pulses (preferably in the femtosecond range or faster) directed at grating 250 which, by diffraction, spreads the pulse in the spatial domain according to its spectral components. (It will be understood that other suitable diffractive means can be utilized herein where gratings are described.) Briefly, the real-time hologram at 240 is read, a line at a time in this embodiment, and, after Fourier transformation by lens L1, converted to the spectral domain by grating 255. The optical field behind the hologram is inverse Fourier transformed by lens L2 and diffracted by grating 255 to

obtain the desired temporal signal and pulse which are, as shown, coupled into fiber optical transmission line 260.

At the receiver, the temporal signals are converted back to the spectral domain using grating 270, and used to form a real-time hologram at medium 285 via splitter 275 and transformation lens L3. In this embodiment, CW laser 360 is used to read out the real-time hologram, which is Fourier transformed by lens L3 and directed by splitter 275, such that encrypted data (290) can be decrypted by decryption system 500.

The optically encrypted memory subsystem (200, 210) according to an embodiment of the invention is shown in FIG. 2. As used, the original data are encrypted by the use of two random phase codes in the input and the Fourier planes. Because of the nature of one-dimensional temporal signals, it has been found convenient to use a one-dimensional spatial signal. Mathematically this may be exemplified by letting  $g_i(x)$  denote the  $i$ th frame of positive real-valued data to be encrypted. Let  $n_i(x)$  and  $h_i(v)$  denote two independent white sequences that are uniformly distributed on the interval  $[0, 2\pi]$ . Here  $x$  denotes the spatial-domain coordinate and  $v$  denotes the Fourier-domain coordinate. The Figure 2 (a) reference numerals 20 and 40 represent coded phase plates operating respectively in the spatial and frequency domains, and lenses 30 and 35 represent, respectively, conversion to the Fourier domain and then the inverse, that is, back to the spatial domain. In the encryption process the input data are illuminated by a collimated light beam and these are then multiplied by a random phase function  $\exp\{-jn_i(x)\}$ . The Fourier transform of the input data is multiplied by another random phase function,  $H_i(v) = \exp\{-jh_i(v)\}$  and is written by

$$E_i(v) = G_i(v)H_i(v) \quad (\text{Equation 1})$$



wherein

$$G_i(v) = F[g_i(x) \exp\{-jn_i(x)\}] \quad (\text{Equation 2})$$

In the above equation 2,  $F\{\cdot\}$  denotes the operation of Fourier transform. These Fourier-transformed encrypted data are stored holographically, together with a reference beam, in a volume storage material (which are well-known) such as a photorefractive material. In order to provide for the storage of many frames of data, angular multiplexing or some other alternative may be employed. The total intensity distribution,  $\Phi(v)$ , is given by

$$\phi(v) = \sum_i^M |E_i(v) + R_i(v)|^2 \quad (\text{Equation 3})$$

Wherein M is the total number of stored frames and  $R_i(v)$  is a reference beam with a specific angle used to record the  $i$ th encrypted data. In the photorefractive material the refractive-index distribution is modulated according to this intensity distribution to store as volume holograms [see, for example, the discussion in The Physics and Applications of Photorefractive Material, Oxford, Clarendon Press, 1996]. In accordance with the presently described system, the erasure of holograms due to the multiple recording is neglected. An appropriate angular separation between adjacent stored data will suppress the cross talk in the reconstructed data, because the stored frames of data create volume holograms.

In the readout process, (Figure 2 (b)), a readout beam is the reference beam. In Figure 2 (b), the lenses 70 and 90

perform the inverses of the lens functions in Figure 2 (a). The  $i$ th reconstructed frame of the stored data is given by

$$r_i(x) = [g_i(x) \exp\{-jn_i(x)\}] \otimes F[\exp\{-jh_i(v)\}] \quad (\text{Equation 4})$$

wherein  $\otimes$  denotes convolution. This encrypted signal is converted into a temporal encrypted signal by use of the space-to-time converter, as described below, before being transmitted through an optical fiber.

An optical transmitter based on the space-to-time converter as shown in FIG. 3 (the transmitter portion of Figure 1) has been previously analyzed by Sun et al. [see IEEE J. Quantum. Electron. 28:2251 (1998)]. Using their analysis, an output temporal signal carrying the encrypted data can be derived. In the present invention, a complex value notation was introduced here simply because optical encryption generates complex data. A spatially collimated and temporally transformed limited optical pulse can be written as

$$s(t) = p(t - t_0) \exp(j\omega_0 t) \quad (\text{Equation 5})$$

wherein  $p(t)$  is the envelope of the pulse,  $t_0$  is the time of the peak intensity, and  $\omega_0$  is the central temporal angular frequency of the pulse. The temporal angular frequency distribution is calculated by taking the temporal Fourier transform of Equation 5:

$$S(\omega) = P(\omega - \omega_0) \exp\{-j(\omega - \omega_0)t_0\} \quad (\text{Equation 6})$$

wherein  $P(\omega)$  is the temporal Fourier-transformed  $p(t)$ .

If the angular frequency response of the space-to-time converter described in FIG. 3 is considered, it can be conceived that a grating is arranged to diffract the light pulse with central angular frequency of  $\omega_0$  into the direction of the optical axis. When a monochromatic plane wave with an angular frequency of  $\omega$  is incident at an angle of  $\omega$  against the grating, the diffracted optical field at the plane P1 will be given by

$$\psi_1(x;\omega) = \exp\left\{-j\frac{\omega - \omega_0}{c}\alpha x\right\}w(x) \quad (\text{Equation 7})$$

wherein  $\alpha = \sin\theta$ ,  $w(x)$  is a pupil function of the grating, and  $c$  is the speed of light in a vacuum. In this instance, the optical field at P2 can be obtained after taking the spatial Fourier transform of Equation 7 by lens L1, and is written by:

$$\psi_2(\eta;\omega) = W\left\{\frac{\omega\eta}{2\pi f} + \frac{\omega - \omega_0}{2\pi c}\alpha\right\}, \quad (\text{Equation 8})$$

wherein  $W(\eta)$  is the spatial Fourier transform of  $w(x)$ ,  $\eta$  is the Cartesian coordinate in the plane P2, and  $f$  is the focal length of lens L1. Equation 8 shows that the Fourier spectra in the Fourier plan is a function of the angular frequency of light. When the pupil function  $w(x)$  is infinite, i.e.,  $W(\eta) = \delta(\eta)$ , the relation between  $\eta$  and  $(\omega - \omega_0)$  and is given by

$$\eta = -f\alpha\frac{\omega - \omega_0}{\omega}. \quad (\text{Equation 9})$$

The spatially spread spectra are modulated by a hologram recorded by the Fourier transform of the encrypted signal described in Equation 4 and a reference beam.

The hereof description assumes that the encrypted signal  $r_i(x)$ , described in Equation 4, was sampled at an interval of  $\Delta$  in the input plane. This data sampling was required to avoid any overlap between adjacent data in the reconstructed spatial data at the receiver because of the point-spread function of spatial-temporal converters [as described in Appl. Opt. 37:2858 (1968)]. As mathematically described below, the spatial data after the transmission of spatial-temporal converters become broad at the receiver. The sampled encrypted signal is given by

$$\begin{aligned} r'_i(x) &= \sum_n r_i(x) \delta(x - n\Delta) \\ &= \sum_n A_i(x) \exp\{j\phi_i(x)\} \delta(x - n\Delta) \\ &= \sum_n A_i(n\Delta) \exp\{j\phi_i(n\Delta)\} \delta(x - n\Delta) \end{aligned} \quad (\text{Equation 10})$$

wherein  $A_i(x) = |r_i(x)|$  and  $\exp\{j\phi_i(x)\} = r_i(x)/|r_i(x)|$ . A spatial Fourier transform of the encrypted input signal by lens L2 is given by

$$R_i(\eta) = \sum_n A_i(n\Delta) \exp\{j\phi_i(n\Delta)\} \exp\left(-j \frac{n\Delta \omega'}{cf} \eta\right) \quad (\text{Equation 11})$$

wherein  $\omega' = 2\pi c/\lambda', f$  is the focal length of lens L2, and  $\lambda'$  is the wavelength of the light beam used to write the resulting hologram. This signal was recorded as the real-time hologram in a storage medium, such as a multiple-quantum-well photorefractive device or higher-order nonlinear material. A hologram was created by the encrypted data described in Equation 11 and a reference beam. Assuming that the hologram works as a grating with the transmittance of

$$t_i(\eta) = \sum_n A_i(n\Delta) \exp\{j\phi_i(n\Delta)\} \exp\left(-j \frac{n\Delta\omega'}{cf} \eta\right) \quad (\text{Equation 12})$$

In which the effect of the carrier frequency of the hologram caused by the angle of the encrypted data and the reference beam was neglected.

The temporal signal in Equation 8 is modulated by the hologram described in Equation 12. The optical field behind the hologram is expressed by

$$\begin{aligned} \psi_3(\eta; \omega) &= \psi_2(\eta; \omega) t_i(\eta) \\ &= W \left\{ \frac{\omega\eta}{2\pi cf} + \frac{\omega - \omega_0}{2\pi c} \alpha \right\} \times \sum_n A_i(n\Delta) \exp\{j\phi_i(n\Delta)\} \exp\left(-j \frac{n\Delta\omega'}{cf} \eta\right) \end{aligned} \quad (\text{Equation 13})$$

This modulated field was then Fourier transformed by lens L2, and this provides for the following equation:

$$\psi_4(X; \omega) = \sum_n A_i(n\Delta) \exp\{j\phi_i(n\Delta)\} \exp\left\{j \frac{\omega - \omega_0}{c} \alpha \left(X + n\Delta \frac{\omega'}{\omega}\right)\right\} w\left(-X - n\Delta \frac{\omega'}{\omega}\right) \quad (\text{Equation 14})$$

This optical field was diffracted again by a grating and is given by

$$\psi_5(X; \omega) = \sum_n A_i(n\Delta) \exp\{j\phi_i(n\Delta)\} \exp\left\{j \frac{\alpha n\Delta (\omega - \omega_0) \omega}{c} \right\} w'\left(-X - n\Delta \frac{\omega'}{\omega}\right) \quad (\text{Equation 15})$$

wherein  $X'$  is the coordinate as shown in FIG. 3 and  $w'(X')$  is the pupil function of the grating projected onto the  $X'$  coordinate.

The output temporal signal may be obtained by taking an

inverse temporal Fourier transform of  $\psi_s(X', \omega)S(\omega)$  that is written by

$$\begin{aligned} o_s(X', t) &= \int_{-\infty}^{\infty} \psi_s(X'; \omega) S(\omega) \exp(-j\omega t) d\omega \\ &= \sum_n A_s(n\Delta) \exp\{j\phi_s(n\Delta)\} \exp\left\{-j\left(X' - n\Delta\right)\frac{\omega}{\omega_0}\right\} p(t - t_0 + n\delta) \exp(j\omega_0 t) \end{aligned} \quad (\text{Equation 16})$$

wherein  $\delta = (\alpha\Delta/c) \times (\omega'/\omega_0)$ . To do this, the following approximation was used:

$$\frac{1}{\omega} = \frac{1}{\omega_0 + \Delta\omega} = \frac{1}{\omega_0} \left( \frac{1}{1 + \Delta\omega/\omega_0} \right) \approx \frac{1}{\omega_0} \left( 1 - \frac{\Delta\omega}{\omega_0} \right) \approx \frac{1}{\omega_0} \quad (\text{Equation 17})$$

to derive Equation 16 because  $\Delta\omega = (\omega - \omega_0) \ll \omega_0^2$  in a few hundreds femtosecond pulse and the center angular frequency of  $2\pi \times 10^{14}$ .

A light pulse, which is passing through the storage medium without diffraction, because of the hologram, has the same envelope as the input pulse; and thus it can be written as

$$s_r(t) = p(t - t_0) \exp(j\omega_0 t) \quad (\text{Equation 18})$$

This pulse may be used as a reference pulse. The temporally encrypted signal described in Equation 16 and the reference pulse in Equation 18 were sent to the receiver through a single-mode fiber to eliminate any distortion that was due to the fiber at the receiver. Both pulses were preferably separated by a delay line before the fiber.

At the receiver the temporally encrypted data were converted into spatially encrypted data by use of a time-to-space converter. Because a single-mode fiber is used to send the temporally encrypted pulse and the reference pulse, the

spatial information of both pulses should be dropped. As shown in FIG. 4, the two light pulses are diffracted by a grating and then form a hologram after being spatially Fourier transformed by Lens L3.

In considering the temporal angular frequency domain with Equations 3, 16, and 18, the intensity distribution of the interference pattern at the Fourier plane P5 is described by

$$\begin{aligned}
 I_i(\eta, \omega) = & \left| O_i(\omega)W \left[ \frac{\omega\eta}{2\pi cf} + \frac{\omega - \omega_0}{2\pi c} \alpha \right] + S_r(\omega)W \left[ \frac{\omega\eta}{2\pi cf} + \frac{\omega - \omega_0}{2\pi c} \alpha \right] \right|^2 = \\
 & |O_i(\omega)|^2 \times \left| W \left[ \frac{\omega\eta}{2\pi cf} + \frac{\omega - \omega_0}{2\pi c} \alpha \right] \right|^2 + |S_r(\omega)|^2 \times \left| W \left[ \frac{\omega\eta}{2\pi cf} + \frac{\omega - \omega_0}{2\pi c} \alpha \right] \right|^2 \\
 & + O_i^*(\omega)S_r(\omega)W \left[ \frac{\omega\eta}{2\pi cf} + \frac{\omega - \omega_0}{2\pi c} \alpha \right]^2 + O_i(\omega)S_r^*(\omega)W \left[ \frac{\omega\eta}{2\pi cf} + \frac{\omega - \omega_0}{2\pi c} \alpha \right]^2
 \end{aligned}
 \tag{Equation 19}$$

wherein  $W(\eta)$  is the spatial Fourier transform of  $w(x)$ ,  $w(x)$  is a pupil function of the grating,

$$O_i(\omega) = \sum_n A_i(n\Delta) \exp\{j\phi_i(n\Delta)\} P(\omega - \omega_0) \exp\{-j(\omega - \omega_0)(t_0 - n\Delta)\}
 \tag{Equation 20}$$

and

$$S_r(\omega) = P(\omega - \omega_0) \exp\{-j(\omega - \omega_0)t_0\}.
 \tag{Equation 21}$$

In this instance, the time separation between the reference pulse and the  $n$ th data pulse is  $nt$ . For purposes hereof, it is assumed that the thin hologram was created by the interference pattern between the reference pulse and the encrypted data pulse, provided that the optical power of the reference pulse is much larger than that of each data pulse.

The third term of Equation 19 is used to reconstruct the spatially encrypted signal. A cw laser beam is incident at the hologram to read out the stored data. The reconstructed optical field was then spatially Fourier transformed by lens L3. When the pupil function of the grating and a beam width are large, i.e.,  $W(\eta) = \delta(\eta)$ , the reconstructed signal at plane P6 is expressed by

$$\xi_i(x') = F \left[ \sum_n A_i(n\Delta) \exp\{-j\phi_i(n\Delta)\} \right] P(\omega - \omega_0)^2 \exp\{-j(\omega - \omega_0)n\delta t\} \quad (\text{Equation 22})$$

With Equations 9 and 17, Equation 22 is calculated as follows:

$$\begin{aligned} \xi_i(x') &= \int_{-\infty}^{\infty} \sum_n A_i(n\Delta) \exp\{-j\phi_i(n\Delta)\} \left[ P(-\omega_0\eta/f\alpha) \right]^2 \exp\{j\omega_0\eta n\delta t/f\alpha\} \exp\{-j2\pi x' \eta/\lambda'' f\} d\eta \\ &= \sum_n A_i(n\Delta) \exp\{-j\phi_i(n\Delta)\} \exp\left\{ -\frac{\alpha^2 \left( \frac{1}{\lambda''} x' + n \frac{\Delta}{\lambda'} \right)^2}{4\omega_0^2 \tau^2} \right\} \end{aligned} \quad (\text{Equation 23})$$

wherein the Gaussian-shaped input pulse envelope written by  $p(t) = \exp(-t^2/2\tau^2)$  is used and wherein  $\tau$  is a pulse width, and  $\lambda''$  is the wavelength of the cw laser beam. Equation 23 shows that each pixel is spread by a Gaussian function with a  $1/e^2$  width of  $w_d = 4\sqrt{2}\omega_0\tau\lambda''/\alpha$ . This signal was used in the following decryption system (see FIG. 5).

When the  $1/e^2$  width of the Gaussian function,  $w_d$  is smaller than the sampling interval,  $\Delta$ , the reconstructed data do not overlap one another. After Equation 21 is sampled at  $x = n\Delta$ , modified reconstructed data are given by

$$\xi'_i(x) = \xi_i(x) \delta(x - n\Delta) = \sum_n A_i(n\Delta) \exp\{-j\phi_i(n\Delta)\} \quad (\text{Equation 24})$$



This equation shows that the complex conjugation of the encrypted signal in Equation 10 is reconstructed. To decrypt the data, the spatial Fourier transform of Equation 24 is multiplied by the phase key  $H(v) = \exp\{-jh(v)\}$ . This phase key was the same random phase mask as that used in the encryption system. In the Fourier plane the reconstructed data are written by

$$\Psi_i(v) = \left\{ G_i^*(v) H_i^*(v) \otimes \exp\left(j \frac{2\pi}{\lambda f} n \Delta v\right) \right\} H_i(v) \quad (\text{Equation 25})$$

wherein  $v$  denotes the coordinate in the Fourier plane P7  $\otimes$  denotes convolution, and  $G_i(v)$  is defined in Equation 2. Finally, the reconstructed data was obtained by taking another Fourier transform by lens L4:

$$I_{out}(x) = \sum_n g_i(x) \exp\{-jn_i(x)\} \otimes F^*[\exp\{-jh(v)\}] \delta(x - n\Delta) \otimes F[\exp\{jh(v)\}] \quad (\text{Equation 26})$$

As discussed below, the error in the decrypted data that is due to the sampling effect may be numerically evaluated.

When  $\omega_0 = 6\pi \times 10^{14}$ ,  $\lambda'' = 1\mu m$ ,  $\alpha = 1/\sqrt{2}$ , and  $\tau = 50 fs$ ,  $w^d$ , is  $754 \mu m$ . If the sampling interval,  $\Delta$ , is smaller than the width of Gaussian distribution,  $w^d$ , in Equation 23, the reconstructed spatial data overlap one another. Thus, the original data cannot be reconstructed when the overlap is large, even if the correct phase key in the decryption process is used.

From J. Opt. Soc. Am. A [15:2629 (1998)] it was pointed out that the double-phase encryption is robust to the occlusion of encrypted data; however, the encryption affects the quality of the recovered data. Therefore undersampling the encrypted

data may cause similar errors in the decrypted data in the system according to the present invention. Thus, the error between the original data and the reconstructed data was numerically evaluated using the sampled encrypted data based on Equation 26. When the encrypted data was undersampled by a factor of 2x, half the encrypted data was lost. By use of binary data it was possible to reduce the noise in the decrypted data by thresholding. A mean-squared error was used as the performance criterion,

$$e = E \left\{ g(x) - m \times g_{\Delta}(x) \right\}^2 \quad (\text{Equation 27})$$

where  $E\{\cdot\}$  denotes statistical average,  $g(x)$  is the original data,  $m$  denotes the coefficient to compensate for the loss of total power due to undersampling the encrypted data, and  $g_{\Delta}(x)$  are the reconstructed data when the encrypted data are sampled at the interval of  $\Delta$ . The original digital data used in the tests are 32-bit data where each bit consists of 64 pixels. Thus, the input data have 2048 pixels. This redundancy of the original data was introduced to recover the original binary data by thresholding of the reconstructed (decrypted) data when there was loss of encrypted data due to sampling. Two random phase codes in the input and the Fourier planes consist of 2048 pixels. The original digital data and the two random phase codes were randomly generated by a computer, and the average mean-squared error was calculated over 1000 different trials. FIG. 6 shows the mean-squared error,  $e$ , as a function of the sampling interval,  $\Delta$ . The error increased as the sampling interval increased. This finding was due to the loss of the encrypted data as  $\Delta$  increases. When  $\Delta=1$ , the original data could be reconstructed without error. FIG. 6 also shows that low-pass filtering of the decrypted data decreased the mean-squared error. The low-

pass filtering was performed by local averaging of the data with a  $1 \times 11$  pixel window. An example of original data, encrypted data, and decrypted data is shown in FIG. 7. Here the decrypted data are low-pass filtered. It can be seen that the encrypted data are randomly encoded, but the decrypted data have the same structure as the original data. Thus, tests indicated that the space-bandwidth product of the original binary data determined whether it was possible to recover the original binary data without error when some of the encrypted data were under-sampled.

The bit error rate as a function of the sampling interval,  $\Delta$ , was also calculated. By using the reconstructed analog data, the energy of each cell of the reconstructed image was calculated. There are a number of methods to threshold the reconstructed output data. To determine the threshold value, all energies were rank ordered. The threshold value was the Nth largest energy of the cells, where N is the number of bright pixels (1's) in the original binary data. This preserved the number of bright pixels between the decrypted data and the original data. FIG. 8 shows the bit error rate as a function of  $\Delta$ . For the binary data described herein, the original digital data were reconstructed without error by application of the computed threshold in the case of  $\Delta = 1$  and 2.

As described herein, the present invention provides for an ultrafast data communication system, using spatial-temporal converters; the proposed system has been analyzed and a numerical evaluation of the effect of sampling of the spatially encrypted data on the quality of reconstructed data has been shown. When the encrypted data were undersampled, the loss of the encrypted data resulted in error in the decryption of data. It is also shown that it was possible to recover the original binary data by thresholding when the pulse width was smaller

than the sampling interval of encrypted data and the sampling interval was short. When the incorrect phase mask was used in the decryption process, the original data was not able to be reconstructed. The system according to the present invention has the potential to implement data transmission with high security and an ultrafast transfer rate.

Accordingly, optical temporal-to-spatial and spatial-to-temporal converters using ultrashort pulses have been investigated because of extremely high converting speed at Tbit/s. As the temporal signal can be sent through an optical fiber, there are possible applications to high speed optical information processing or database systems based on these converters.

In summary, in the present invention, an ultrafast secure data secure data transmission using time-to-space converters has been described. The spatial original data is encrypted by using double random phase encoding and is then stored in an optical storage material as shown in FIG. 2. (Multi-dimensional keys can be used to make the system more secure.) The spatial data readout from the storage material is converted into a temporal signal by using a space-to-time converter.(Figures 1 and 3). This temporal encrypted data is transmitted through an optical fiber. In the receiver the temporal encrypted signal is converted into a spatial signal and is then decrypted. In the decryption it is necessary to use the correct phase key in the Fourier plane for successful retrieval of the original data (Figures 1, 4, and 5). The correct key is the same as the random phase mask used in the Fourier plane in the encoding process.

The encryption and decryption in the proposed system was evaluated by numerical technique. The size of pixel of encrypted data in the receiver is expanded in proportion to the

width of the optical pulse due to the space-to-time and time-to-space converters. Thus the need to sample the encrypted data to avoid overlapping between adjacent pixels in the receiver. That the original digital data was recovered even when the encrypted data was undersampled was confirmed .

Figure 1: Schematic diagram of the proposed system. The system consists of a transmitter and a receiver. The transmitter takes a digital input and converts it into an optical signal using a space-to-time converter. This signal is then encrypted using a key stream. The encrypted signal is transmitted through a channel. The receiver receives the signal and decrypts it using the same key stream. Finally, a time-to-space converter converts the decrypted signal back into a digital output.